Seismic Evaluation of Dome Structure for Different Zones

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ABSTRACT

'Dome' is a component of architecture that bears a resemblance to a void upper part of a sphere. It is erected using an assortment of materials which will have a longer 'architectural- lineage' that will extend into prehistory. It may be also defined as a thin- shell that is generated by the revolving a normal curve about one of its common axis. The outline of the dome depends on the type of the 'curve' & the path of revolving axis. When the part of a 'regular curve' orbits about its own vertical diameter, a spherical geometrical shape is generated. These structures are used in various kinds of structures like circular shaped roof, circular shaped tanks, exhibition halls, auditorium areas, bottom part of tanks & bunkers. With the introduction of monolithic- domes wide applications were done in many subdivisions of engineering & technology. From the view point of an architect, the growth of dome proffers unexpected opportunities & openings for the combinations of awareness of functional plus economic & also aesthetic facets. Energy-efficiency of any building designs need a consideration and is it lofty in this type monolithic dome component. A monolithic cast dome is a structure component that is cast in a 'one-piece' form. The form work may be permanent as well as temporary & mayor may not stay as a part of the final structure. Monolithic is bestowed to improve individual's lives globally. By bringing in & casting monolithic Domes for both personal as well as public use that are calamity resistant, 'energy efficient' & also cost- effective.

INTRODUCTION

Domès 1st came into viewed as solid-mounds & in tèchniques that is adaptablè only for a smallèst sizèd building like round shapèd huts & tombs in thè anciènt times in Middle East and India and also in Mèditerranean. The Románs brought in the 'largèr sixed' masonry hèmi-sphere or domès& the original monumental samplè like the Roman Panthèon needed a hèavy and strongsupporting wall.

'Byzantine' architècts inventèd a procedure to raisè theses domès on piers by lètting lighting & communication from all the 4 dirèctions. The changè from a cubical support to the hèmispherical shapèd domè was accomplishèd by 4 pendent, invèrted triangular set of masonry massès that is vertically as wèll as horizontally curvèd. Their bottoms were placèd on the 4 vèrtical columns to which forcès from the domè they conducted, their sidès were connected so that archès are crèated over available opènings between thèse columns on the 4 sidès of thè cubè and *How to cite this paper*: Harshita S R | Dr. Eramma H "Seismic Evaluation of Dome Structure for Different Zones"

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thèir bottoms were madè such a way that thèy make a complète circle that acts as a foundation for the domè. The pendant- domè could be placed on its circular foundation dirèctly or on a cylindrical shapèd wall which is callèd as drum which is insèrted in bètween the twò to augment height.

Displaced by the light architecturally,. Vertical styles Gothic-architècture the domè rèsumed of attractivèness during the 'Europèan Renaissance' & 'Baroque times'. The yearning to observe convention protected the domè in thè èarlier iron & steel time. The contemporary R,C slab used in the vaulting & domès had vanished from its unusual worth bèing based barely on the type of bend in the slab. In thisstudy thè 'Gèodesic' Domè is analyzed & it is built-up of triangulár & polygonál plates thát contributè in the distribution of strèsses within the structure. It is erected as a 'load bearing' structure with the stabilising components that can uphold both horizontal International Journal of Trend in Scientific Research and Development @ www.ijtsrd.com eISSN: 2456-6470

& vèrtical loads. The structurè must be strong & satisfactorily designèd against any structural failurè, cracks& damaging dèformations.

Objectives of the Study

The key/main goal of the work is to analyse a domè structurè such as shèll structure, ring-beam, column & the reactions at base-level.

- 1. To study & analyse Monolithic-Concrete Domè using STAAD-Pro.
- 2. To analyse the model for zone —II & V carrying load likes dead, live and seismicload.
- 3. To create two models & compare for zone —II & V by providing bracings to keepthe displacement within the limit.

DEFINING THE PROBLEM

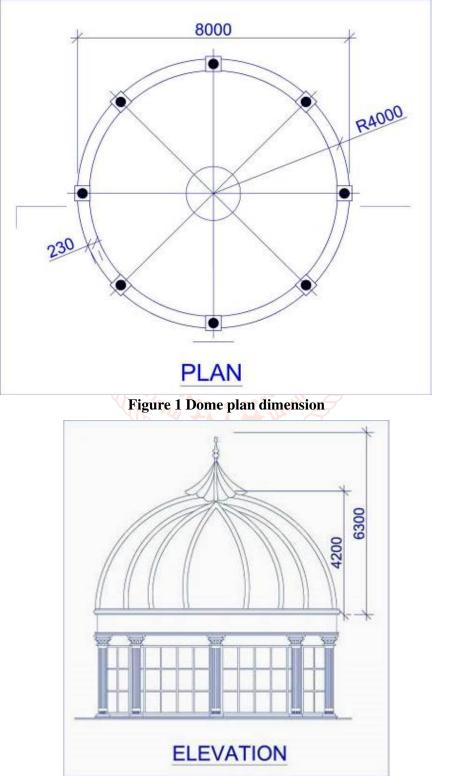


Figure 2 dome elevation & heights

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METHODOLOGY

The 'meditation hall' domè is analyzed and then check designed is carried out. All the members are designed with the column as fixed. The methodology followed for this domè & their components design are shown below.

- 1. CREATING THE DRAWING AS PER THE DIMENTION NEEDED
- 2. CREATING THE MODEL IN STAAD AS PER THE CAD
- 3. CREATE & APPLYING THE MATERIALS
- 4. APPLYNG THE END CONDITIONS AT BASE
- 5. GENERATNG THE PRIMRY LOADS AND THEIR COMBINATIONS
- 6. APPLYNG THESE PRIMRY LOADS
- 7. PERFORMING THE ANALYSIS
- 8. PERFORMING DESIGN OF SHELL TO ENSURE SECTIONS ARE ENOUGH
- 9. DESIGN OF ŔING BEAM TO ENSURE SECTIONS ARE ENOUGH

10. DESIGN OF COLUMN TO ENSURE SECTIONS ARE ENOUGH

RESULTS AND DISCUSSION

Absolute displacement in X

In STAAD Pro, absolute displacement is a value that can be specified as a displacement control for the first analysis step.

| Table 1 | Absolute D | isplacement |
|--------------|--------------|-------------|
| Absolu | ite Displace | ment, mm |
| 1.20(| Dead+Lat- | Load-X) |
| Node | ZoneII | ZoneV |
| 131 | 4.042 | 4.575 |
| 0 144 | 4.039 | 4.572 |
| 118 | 4.035 | 4.573 |
| <u>1</u> 57 | 4.024 | 4.564 |
| 105 | SS 4.0156-6 | 47 4.565 |
| 170 | 3.997 | 4.551 |
| 92 | 3.985 | 4.553 |
| 183 | 3.96 | 4.534 |
| 79 | 3.944 | 4.536 |
| 196 | 3.913 | 4.513 |
| 66 | 3.893 | 4.515 |
| 209 | 3.857 | 4.488 |
| 53 | 3.835 | 4.491 |
| 222 | 3.794 | 4.461 |
| 40 | 3.769 | 4.464 |
| 235 | 3.725 | 4.433 |
| 27 | 3.699 | 4.435 |
| 248 | 3.653 | 4.301 |
| 13 | 3.625 | 4.306 |
| 14 | 3.614 | 4.306 |
| 261 | 3.578 | 4.273 |
| 469 | 3.55 | 4.276 |
| 274 | 3.504 | 4.145 |
| 456 | 3.477 | 4.147 |
| 287 | 3.432 | 4.018 |
| 443 | 3.407 | 4.032 |
| 300 | 3.365 | 4.013 |
| 430 | 3.343 | 3.95 |
| | | |

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| 313 | 3.306 | 3.902 |
|-----|-------|-------|
| 417 | 3.287 | 3.914 |
| 326 | 3.257 | 3.906 |
| 404 | 3.242 | 3.857 |
| 339 | 3.219 | 3.643 |
| 391 | 3.209 | 3.644 |
| 352 | 3.195 | 3.536 |
| 378 | 3.189 | 3.636 |
| 365 | 3.185 | 3.833 |

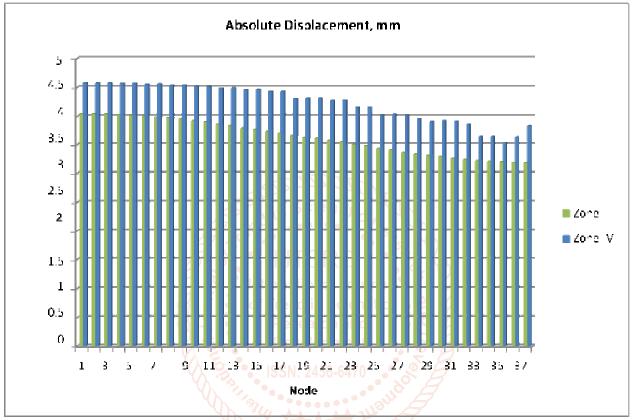
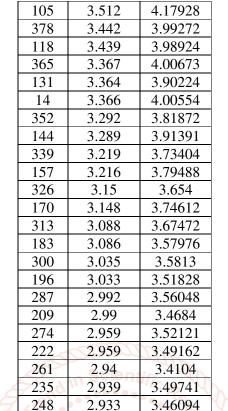


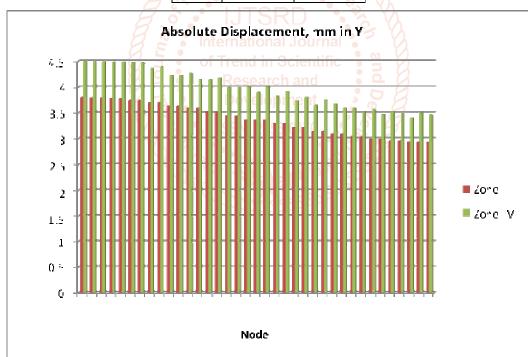
Figure 2 Absolute Displacement Chart in x

Absolute Displacement in Y

Table 2 Absolute Displacement in Y

| DIC 2 AL | solute Disp | |
|----------|--------------|----------|
| Absolu | ite Displace | ment, mm |
| 1.20(| [Dead+Lat-] | Load-Y) |
| Node | ZoneII | ZoneV |
| 13 | 3.798 | 4.494 |
| 469 | 3.791 | 4.492 |
| 27 | 3.791 | 4.491 |
| 456 | 3.772 | 4.484 |
| 40 | 3.771 | 4.483 |
| 443 | 3.741 | 4.472 |
| 53 | 3.739 | 4.471 |
| 430 | 3.698 | 4.36364 |
| 66 | 3.696 | 4.39824 |
| 417 | 3.644 | 4.22704 |
| 79 | 3.642 | 4.22472 |
| 404 | 3.583 | 4.26377 |
| 92 | 3.58 | 4.1528 |
| 391 | 3.515 | 4.1477 |





Base reactions

Table 3 Base Reaction in X

| Ba | se Reaction | n in X |
|-------|-------------|---------|
| 1.20(| Dead+Lat- | Load-X) |
| Node | ZoneII | ZoneV |
| 470 | 6.077 | 7.544 |
| 471 | 17.316 | 21.805 |
| 472 | 26.07 | 30.93 |
| 473 | 20.199 | 26.249 |
| 474 | 6.24 | 8.524 |

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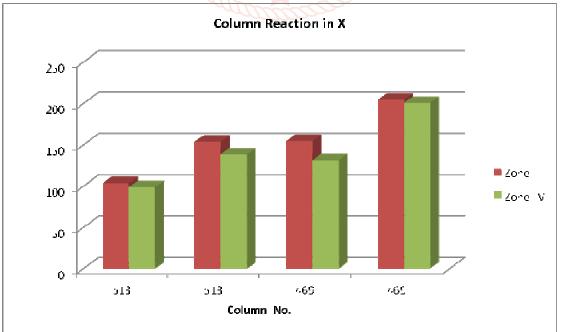
| 475 | 17.2 | 24.027 |
|-----|-------|--------|
| 476 | 15.81 | 24.261 |
| 477 | 19.4 | 23.32 |

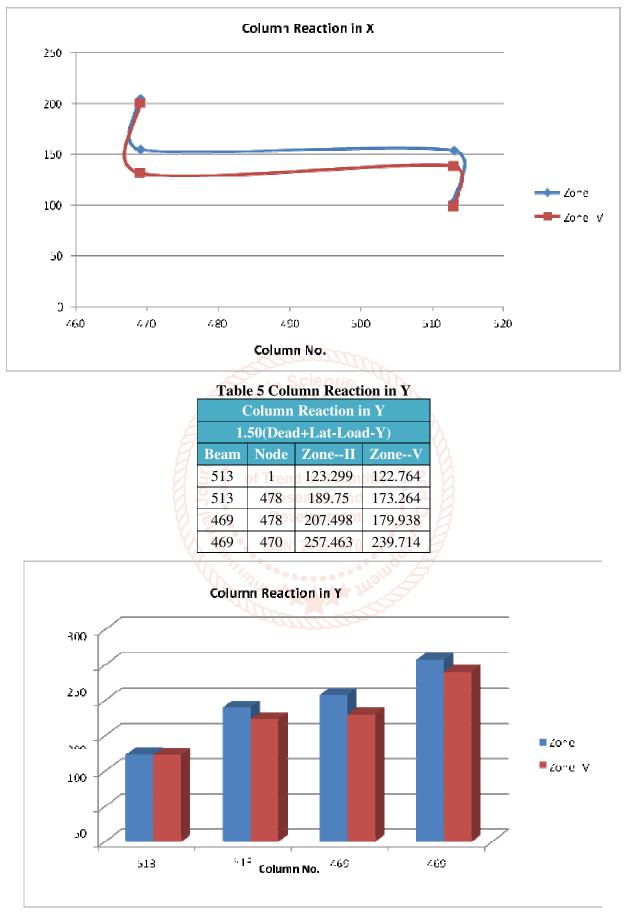
35 30 25 **=** 20 re Zone V 10 ò, 2 3 7, 1 1 6 Z 8 Nodelentific

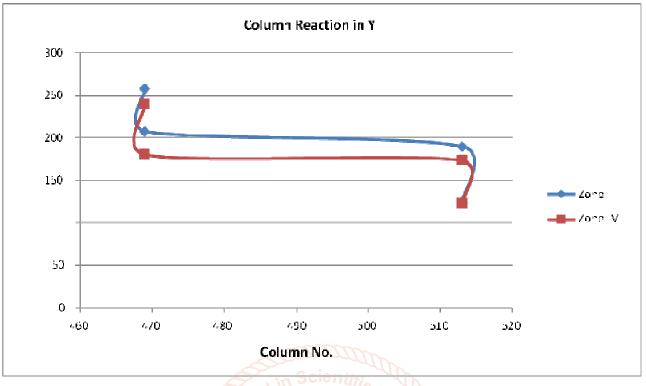
Base Reaction in X

Figure 4 Base Reaction in X Chart

| Table 4 Column Reaction in X Column Reaction in X 1.50(Dead+Lat-Load-X) | | |
|---|--|--|
| | | |
| 1 | 103.913 | 98. <mark>7</mark> 173 |
| 478 | 153.877 | 138.489 |
| 478 | 154.77 | 131.554 |
| 470 | 204.734 | 200.639 |
| | Column 50(Dead Node 1 478 478 | Column Reaction i 50(Dead+Lat-Loa Node ZoneII 1 103.913 478 153.877 478 154.77 |







CONCLUSION

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We analyzed monolithic RC Domès as per the [1] Mohamed Imran. S1, Dr. R. Thiyagarajan2 - standard codes and conclusions were drawn as below. 2022

For model in zone —II when analyzed various analysis on [2] Lian Máng Chèn, Kái-Yu Huáng, Yi Jie Liu, results like drift, displacement etc were checked and in Scien Yi Hong Zeng, Ze Bin Li, Yi Yi Zhou&Shi found to be within the limits. However, these were arch and Lin Dong - 2023

slightly crossing acceptable limits in zone -V. The [3] Yuan; Chen & Dong; Zhang; & Liang, Dong, reason for this is rise in seismic intensity. To take care of this, bracings were added as shown above and we 2456-6470 & Miao - 2007

were able to bring the results down below the recommended limits. Below we have explained the results with their values

From the above results it is observed that the average lateral Displacement (X) is found to be more for zone -V model (4.22 mm) which is 3.63 mm zone -II model and in Y directionit is 3.96 mm for zone -V then 3.37 mm for zone -II model. So both in X & Y value is more forzone -V model (X dir - 17% more and Y dir - 18% more than zone -II model). However, it is still within the allowed limit.

Similarly the base reaction for zone -V model in x is 20.83 kN (avg.) and in Y it its 9.69 kN (avg.). For zone -II it is 16.04 kN (avg.) in X & 8.54 kN (avg.) in Y. Percentage wise in X it is 31.1% more & in Y the same is 28% for zone -V model than zone -II model.

The stress observed are slightly more in case of zone -V model than the one in zone -II for the obvious reason that the intensity of earthquake is more. However, this can be addressed in design part as these are not beyond permissible limit.

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