

Investigation on Appropriateness of Turbo-matching of B60J68 and A58N70 Turbochargers for a Commercial Vehicle

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ABSTRACT

Nowadays turbo-chargers preferred for are commercial vehicle especially to ensure the good operating conditions at higher loads. Turbo-matching is a complex task and carried out by many methods. Recent manufacturing trend added many components in supplier chain. This piece of investigation adopts test based methodologies to perform such matching. The simulation is used to predict the operating conditions at various speeds. The same verified with data-logger method which is like on road test. The routes preferred for evaluating the various routes namely rough road, highway matching performance are: Rough Road, Highway, City Derive, slope up and slope down. The compressor map used for analyse the appropriateness of matching by methods and suggesting the appropriate turbocharger.

Keywords: turbo-matching; turbo-charger; chock; surge; simulation; data-logger;

I. Introduction

Turbo charger is an accessory in the IC engines to boost pressure, especially at higher loads. Turbo charger also helps to reduce specific fuel consumption (SFC), downsizing the engine, reduce CO_2 emission, etc.[1]-[5]. Due to the character of centrifugal compressor, the turbocharged engine yields lesser torque than naturally aspirated engine at lower speeds [6],[7]. Comparatively in diesel engine these problems very worse than petrol engine. Some of the system designs were made to mange this problem. They are: adopting the sequential system [8], incorporate the limiting fuel system, reducing the inertia, improvements bearing, modification on on aerodynamics [9], establishing electrically supported turbocharger [10], the usage of positive displacement charger i.e., secondary charging system and use of either electric compressor or positive displacement charger with turbocharger [10],[11] facilitating the geometrical variation on the compressor and turbine [12], adopting the twin turbo system [13], and dual stage system [14]. It is noticed that the transient condition is always worst with the engine which adopted single stage turbo charger. The variable geometry turbine was introduced for reducing the turbo lag in petrol as well as diesel engines. But the system is not exact match for petrol engines [15]. Even though many research were done on this case still the problem is exist. [12],[15]-[18]. Though the advancements in system design like variable geometry turbine, common rail injection system, and multiple injections, the problem is still persist due to the limiting parameter say supply of air. [19] discussed in detail about the benefits, limitations of turbo charger in single stage, parallel and series arrangements. According to the literature the turbocharger matching is a tedious job and demands enormous skill. The turbo matching can be defined as a task of selection of turbine and compressor for the specific brand of engine to meet its boosting requirements. That is, their combination to be optimized at full load. The trial and error method cannot be adopted in this case because the matching is directly effects as well as affects the engine performance [5], [20], [21]. So it is difficult task and to be worked out preciously. If one chooses the trial and error or non precious method, it will certainly lead to lower power output at low speeds for partly loaded engines for the case of two stage turbo charger. It is because of the availability of a very low pressure ratio after every stage than single stage [21]. Some cases the turbocharger characteristics are not readily available, and in some cases, not reliable or influenced by the engine which is to be matched [19]. Nowadays the Simulator is used for matching the turbocharger to the desired engine. The simulator was used to examine the performance at constant speed of 2000 rpm of two stage and single stage turbo chargers, the aim of the study was to optimize the high load limit in the Homogeneous charge compression ignition engine. For increasing the accuracy of matching the test bench method is evolved. Test bench was developed and turbo mapping constructed for various speeds to match the turbocharger for the IC engine by Leufven and Eriksson, but

It is a drawn out process [21]. The on road test type investigation is called Data Logger based Matching method is adopted in this research. [22] discussed the data-logger turbocharger matching method in detail and compared with the result of test best method and simulator based matching method. And proved the data logger method outputs are reliable. By use of the data logger method the performance match can be evaluated with respect to various speeds as well as various road conditions. The core objective of this research is investigating the appropriateness of matching of the turbocharger with B60J68 and A58N70 for the TATA 497 TCIC -BS III Engine by simulator method. The validation of the same by Data Logger based Matching method.

II. Materials and Methods

A logical science of combining the quality of turbocharger and engine and which is used to optimize the performance in specific operating range is called as turbo-matching. The Simulation, datalogger method and Test Bed method identified for this evaluation. Apart from the above three this research used the Simulation and data-logger method for evaluating the performance of turbo matching. The trim size is a parameter, which can be obtained from the manufacture data directly or by simple calculation. That is the trim size is a ratio of diameters of the inducer to exducer in percentage. This parameter is closely related to the turbo matching. Various trim sizes are available, but in this study the trim size 68 and 70 are considered for investigation.

A. Simulator Based Matching

Various kinds of simulation software are being used for turbo matching. In this research the minimatch V10.5 software employed for turbo-matching by simulation. The manufacturer data of the engine and turbocharger are enough to find the matching performance by simulation. The manufacturer data are like turbo configuration, displacement, engine speed, boost pressure, inter cooler pressure drop and effectiveness, turbine and compressor efficiency, turbine expansion ratio etc. The software simulates and gives the particulars of the operating conditions like pressure, mass flow rate, SFC, required power etc. at various speeds. These values are to be marked on the compressor map to know the matching performances. The compressor map is a plot which is used for matching the engine and turbocharger for better compressor efficiency by knowing the position of engine operating points. Based on the position of points and curve join those points the performance of matching will be decided.

B. Data Logger based Matching

This type of data collection and matching is like on road test of the vehicle. This setup is available in the vehicle with the provision of placing engine with turbocharger and connecting sensors. It is a real time field data gathering instrument called as Data-logger. It is a computer aided digital data recorder which records the operating condition of the engine and turbo during the road test. The inputs are gathering from various parts of engine and turbo charger by sensors. The Graphtec make data logger is employed in this work. It is a computerized monitoring of the various process parameters by means of sensors and sophisticated instruments. The captured data are stored in the system and plot the operating points on the compressor map (plot of pressure ratio versus mass flow rate). The Fig. 1 depicts the setup for the data-logger testing in which the turbocharger is highlighted with red circle.

C. Decision Making

The decision making process is based on the position of the operating points on the compressor map. The map has a curved region like an expanded hairpin, in which the left extreme region is called surge region. The operating points fall on the curve or beyond, is said to be occurrence of the surge. That means the mass flow rate limit below the compressor limit. This causes a risk of flow reversal. The right extreme region curve is called as Choke region. The points fall on the curve and beyond its right side is denoted as the occurrence of choke. In the choke region the upper mass flow limit above compressor capacity, which causes the quick fall of compressor efficiency, Chances for compressor end oil leakage and insufficient air supply. The all operating points fall in between those extreme regions i.e., the heart region holds good. It must be ensured at all levels of operation of the engine holds good with the turbocharger. The manufacturer of Turbocharger provides the compressor map for each turbo charger based on its specifications.

D. Engine Specifications

Table I: Specification of Engine

Description	Specifications				
Fuel Injection Pump	Electronic rotary type				
Engine Rating	92 KW (125 PS)@2400 rpm				
Torque	400 Nm @1300-1500rpm				
No. of Cylinders	4 Cylinders in-line water cooled				
Engine type	DI Diesel Engine				
Engine Bore / Engine Stroke	97 mm/128mm.				
Engine speed	2400 rpm (Max power), 1400 rpm (Max Torque)				

The TATA 497 TCIC -BS III engine is a common rail type diesel engine. It is commonly used for medium type commercial vehicle like Tata Ultra 912 & Tata Ultra 812 trucks. The engine develops 123.29 BHP at 2,400 rpm and also develops the peak torque of 400 Nm between 1,300 and 1,800 rpm. The other specifications can be found in Table 1.

E. Turbochargers Specifications

The TATA Short Haulage Truck, turbochargers of B60J68 and A58N70 are considered to examine the performance of matching for TATA 497 TCIC -BS III engine. For example, if specification A58N70 means in which the A58 is the design code and N70 is the

Trim Size of the turbocharger in percentage. The other specifications furnished in Table 2.

Table II: Specification of Turbo Chargers

Description	B60J68	A58N70
Turbo maximum Speed	200000 rj	om
Turbo Make	HOLSET	
Turbo Type	WGT-IC with Inter	(Waste gated Type cooler)
Trim Size (%)	68	70
Inducer Diameter	46.9mm	48.6 mm
Exducer Diameter	68.9 mm	69.4 mm

III. Experimental Observation

The simulation and data-logger method is adopted to match the Turbo Chargers B60J68 and A58N70 for TATA 497 TCIC -BS III engine. The matching performance is obtained by simulation by using the data from the manufacturer catalogue. The desired combination is simulated at various speeds (1000, 1400, 1800 and 2400 rpm) to obtain the predicted operating conditions for this combination. The Pressure ratio and mass flow rates are important parameters to know the turbo matching performance. The simulated observations presented in the Table 3 for B60J68 and A58N70 Turbo matching. In datalogger method the turbocharger is connected to the TATA 497 TCIC -BS III Engine of TATA 1109 TRUCK with sensors. The vehicle loaded to rated capacity 7.4 tonnes of net weight. The grass weight of vehicle is 11 tonnes. The experimental setup for Data logger type matching is shown in

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Table VI



Fig. I Data-Logger method Experimental set up

Tabl obse	Table V Data-logger – Highway Route observations						
S. No	Engine Speed (rpm)	Mass Flow Rate (Kg/sec.sqrt K/Mpa)		Pressure	e Ratio		
		<i>B60J68</i>	A58N70	<i>B60J68</i>	A58N70		
1	1000	8.12	8.52	1.35	1.31		
2	1400	15.92	16.39	1.95	1.87		
3	1800	21.87	23.94	2.33	2.3		
4	2400	27.87	28.91	2.56	2.51		

Data-logger - City Drive observations

Pressure Ratio

A58N70

1.32

1.95

2.33

2.56

B60J68

1.36

1.95

2.35

2.59

Table IIISimulated observations

S.N Engin o e Speed		Mass Flow Rate (Kg/sec.sqrt K/Mpa)		Pressure Ratio		S. No	Engine Speed (rpm)	Mass Flow Rate (Kg/sec.sqrt K/Mpa)	
	(rpm)	<i>B60J6</i>	A58N7	<i>B60J6</i>	A58N7			<i>B60J68</i>	A58N70
		8	0	8	0	1	1000	7.41	8. <mark>49</mark>
1	1000	11.449	9.534	1.856	1.856	2	1400	15.52	16.31
2	1400	22.56	20.186	3.051	3.042	3	1800	21.68	23.78
3	1800	29.451	27.958	3 556	3 548				
5	1000	27.431	21.950	5.550	5.540	4	2400	27.39	28.37
4	2400	36.872	35.488	3.817	3.764				
4	2400	36.872	35.488	3.817	3.764		<u> </u>		

 Table IV
 Data-logger – Rough Road observations

S. No	Engine Speed (rpm)	Mass Flow Rate (Kg/sec.sqrt K/Mpa)		Pressure Ratio		
		B60J68	A58N70	B60J68	A58N70	
1	1000	7.37	8.43	1.35	1.29	
2	1400	15.41	16.27	1.95	1.9	
3	1800	21.73	23.87	2.33	2.29	
4	2400	27.43	28.49	2.55	2.51	

Table VII Data-logger –slope Up observations

S. No	Engine Speed (rpm)	Mass Flow Rate (Kg/sec.sqrt K/Mpa)		Pressure Ratio		
		B60J68	A58N70	B60J68	A58N70	
1	1000	8.02	8.58	1.38	1.31	
2	1400	15.81	16.34	2.00	2.00	
3	1800	21.94	23.98	2.39	2.37	
4	2400	27.97	28.98	2.62	2.58	

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S. No	Engine Speed (rpm)	Mass Flow Rate (Kg/sec.sqrt K/Mpa)		Pressure Ratio	
		B60J68	A58N70	B60J68	A58N70
1	1000	7.97	8.47	1.35	1.30
2	1400	15.79	16.32	1.95	1.95
3	1800	21.76	23.89	2.33	2.31
4	2400	27.41	28.42	2.60	2.50

 Table VIII
 Data-logger – Slope Down observations

Fig 1. The operating conditions collected while driving at a specific speed in the selected route. For the same set of engine speeds the operating conditions were observed while vehicle driving in the routes like Rough Road, Highway, City Drive, Slope up and Slope down. The observations were recorded in the data-logger automatically through sensors. Those data logger observations were tabulated road condition wise from Table 4 to Table 8.

IV. Results and Discussions

The operating conditions obtained for both case of turbo-chargers with engine for both simulator and data-logger method with rough road route, highway route, city drive, slope-up and slope-down route were obtained. These operating conditions were marked on the respective compressor map. The Fig.2 and Fig.3 are for turbo-matching B60J68 turbocharger and A58N70 Turbochargers for TATA 497 TCIC -BS III Engine respectively for both methods especially at Rough Road route condition. Similarly Fig.4 and Fig.5 for Highway route, Fig.6 and Fig.7 for City Drive route, Fig.8 and Fig.9 for Slope up and Fig.10 and Fig.11 for Slope down. It was observed from the compressor maps (Fig.2 to Fig.11) that the both the turbo chargers performing well all speeds at all preferred routes. The simulated values are much higher than the data-logger values. Especially at higher speed the turbo-match is very perfect. In particularly the B60J68 turbocharger's turbo-match, operating condition lower speed is nearby surge line. The turbomatch of A58N70 turbocharger is found safe at all speeds as well as all routes preferred for evaluation. Hence the A58N70 turbocharger can be best match than B60J68 turbocharger.



Fig. II B60J68 Turbo-match-Rough Road



Fig. III A58N70 Turbo-match-Rough Road

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Fig. IV B60J68 Turbo-match - Highway



Fig. V A58N70 Turbo-match- Highway











Fig. VIII B60J68 Turbo-match- City Drive



Fig. IX A58N70 Turbo-match- City Drive







Fig. XI A58N70 Turbo-match- Slope Down

CONCLUSION

The turbo-matching of B60J68 turbocharger and A58N70 turbocharger for TATA 497 TCIC -BS III engine is considered. The turbo-charger B60J68 performs well at all operating fields but its lower speed's operating conditions found nearby the surge region. Because, the operations of vehicle at lower speed, the surge occurs at flow. The same operating performance was observed in simulated solution as well as data-logger method with irrespective of routes. The turbocharger A58N70 operating performance shows that the turbo-match is good at all speeds. As the A58N70 turbo-match satisfy the operating performance on both methods. A58N70 turbo-charger is found match TATA 497 TCIC -BS III engine. The

data-logger method adapted in this research may feel as expensive but it is one time job for finding the best turbo-match for an engine category.

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