Speed Control System of Induction Motor by using Vector Control Method

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The field orientation control of induction motor allows decoupling the control of magnetic flux and the control of the torque produced by the stator current. This makes the induction motor control more akin to the control of the separately excited DC motor. That is, in three phase induction motor control, the rotor field can be equivalent to the field of excitation of dc motor, but with the difference that the voltage in the rotor, which produces the field, is dependent on the magnetic field in the stator.

II. Methods of Vector Control

The way of determining the angle position of the rotor flux vector, rotating at the synchronous speed, depends on the type of the field orientation: either direct field orientation or indirect field orientation.

A. Direct Field Orientation Method

When the identification of the flux vector is done by direct Hall sensor measurement or even indirectly by estimation of other motor electrical variables, it is called direct field orientation. This method depends on measuring the air gap flux using special sensor is called Hall-Effect-Device. The magnetic flux measured is the mutual flux not the rotor flux, which Paper has Dangle- which is Important to be properly oriented. The connection with the known stator current provides the solution of determining this angle. Proportional Integral (PI) controller methodology is used in both the flux and the torque loops to get the desired direct and quadrature components of the stator current in the

ABSTRACT

I.

In the Vector Control method of induction motors, one of the advantages of the separately excited DC motor of being able to decouple the flux control and the torque is thereby opened up. The field orientation control of induction motor allows decoupling the control of magnetic flux and the control of the torque produced by the stator current. To drive three-phase squirrel-cage induction motor with a constant speed, vector control technique is used. In this paper, the development of speed control system for three-phase squirrel-cage induction for proposed system is done with the help of MATLAB/SIMULINK.

KEYWORDS: Field orientation control, three-phase squirrel-cage induction motor, vector control method

INTRODUCTION

Induction motor plays a very important role in both worlds, because of low cost, reliable operation, robust operation and low maintenance. There are two main types of induction motors which are the wound rotor and squirrel-cage motor and both of them are in widespread use. Squirrel-cage rotor winding design is considered more reliable and cheaper to be made. Control of a three-phase squirrel cage induction motor is difficult, because it is not simply about independently controlling the voltage and the frequency only. But the vector control method can perform a faster critically damped response that is non-oscillating.

Development

synchronous reference frame. Those are then transformed to the same component in the stationary frame. Finally the equations of control are referenced to the three phase motor drive currents to control the inverter operating conditions.

B. Indirect Field Orientation Method

For very low-speed operations and for position type control, the use of flux sensing that relies on integration which has a tendency to drift may not be acceptable. A commonly-used alternative is indirect field orientation, which does not rely on the measurement of the air gap flux, but uses the condition in Equations 1 to 3 to satisfy the condition for proper orientation

$$\mathbf{v}_{qr}^{e} = \mathbf{r}_{r} \mathbf{i}_{qr}^{e} + p \lambda_{qr}^{e} + (\omega_{e} - \omega_{r}) \lambda_{dr}^{e} \quad \mathbf{V}$$
1

$$\lambda_{dr}^{e} = \frac{r_{r}L_{m}}{r_{r}+L_{r}p}i_{ds}^{e}$$
 Wb.tum

$$\lambda_{dr}^{'*} = \frac{r_r' L_m}{r_r' + L_r' p} i_{ds}^{e^*} \quad \text{Wb.turn}$$

The above conditions, if satisfied, ensure the decoupling of the rotor voltage equations. To what extent this decoupling is actually achieved will depend on the accuracy of motor parameters used. Since the values of rotor resistance and magnetizing inductance are known to vary somewhat more than the other parameters, on-line parameter adaptive techniques are often employed to tune the value of these

2

ω

parameters used in and indirect field-oriented controller to ensure proper operation.

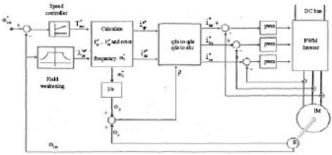


Figure.1 Indirect Field-oriented Control of Currentregulated PWM Inverter Induction Motor Drive

Mathematical Model of Induction Motor III.

There are three main references of motion, which could be used to model the three phase induction machine in its three main regions of operation. These are stationary reference frame for startup, the synchronous reference frame for equilibrium motion, and the rotor reference frame for changing speeds by acceleration or deceleration. The two commonly employed coordinate transformations with the induction machine are the stationary and the synchronous reference frame. These mathematical transformations, which are known as Park Transformation, can facilitate the understanding of the variation of mutual inductance between the stator and the rotor under differing rotation conditions. In this paper, the modeling is done in synchronous reference frame where the variables appear as DC quantities facilitating smooth control. Here, the three phase variables (a-b-c variables) are first transformed into stationary reference frame using Clark's transformation and the d-q axis variables are obtained using Park's arc transformation, there by facilitating controller design and loop evaluation of transient phenomena in the drive system. Figure 2 shows the equivalent circuit of d-q axes of induction 2456 motor.

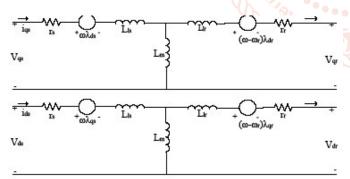


Figure.2 Equivalent Circuit in d-q Axes of Induction Motor

$$V_{qs}^{s} = \frac{2}{3}V_{a} + \frac{1}{3}V_{b} - \frac{1}{3}V_{c} \qquad 4$$

$$V_{ds}^{s} = \frac{\sqrt{3}}{2} V_{b} - \frac{\sqrt{3}}{2} V_{c}$$
 5

$$V_{ds}^{e} = V_{as}^{e} \sin \theta_{e} - V_{ds}^{s} \cos \theta_{e}$$
 7

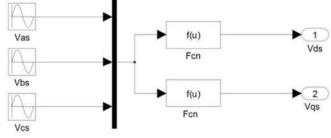
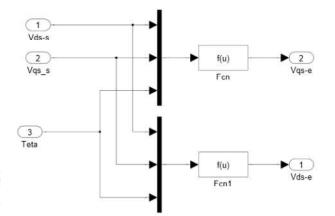
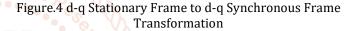


Figure.3 Three-phase to d-q Stationary Reference Frame Transformation



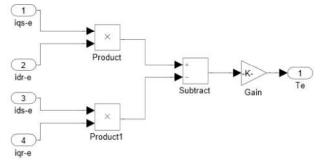


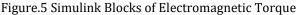
$$\mathbf{r}_{e} = \frac{3}{2} \frac{\mathbf{P}}{2} \mathbf{L}_{m} [\mathbf{i}_{dr}^{e} \mathbf{i}_{qr}^{e} - \mathbf{i}_{qr}^{e} \mathbf{i}_{ds}^{e}]$$

$$T_{e} = T_{L} + B\omega_{m} + J \frac{d\omega_{m}}{dt}$$
 9

$$_{m} = \int_{t=0}^{t} \frac{(T_{e} - T_{L} - B\omega_{m})}{J} dt$$
 10

Where P is the number of pole and T_e is the electromagnetic torque T_L is load torque, J is the inertia of the rotor and connected load B is the friction. The Simulink block of electromagnetic torque is shown in Figure 5 and the Simulink block of motor speed is shown in Figure 6.





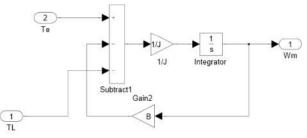
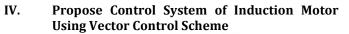


Figure6. Simulink Blocks of Motor Speed



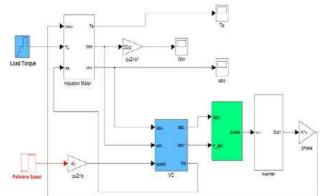


Figure.7 Overall Simulink Model of Vector Control for Induction Motor

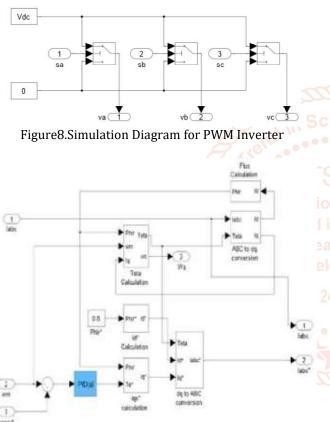


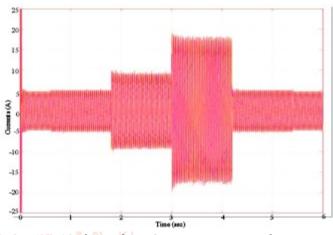
Figure.9 Simulink Model of Vector Control Block

The overall Simulink model of vector control system for induction motor is shown in figure 7. Figure 8 is PWM Inverter generation block and figure 9 is Vector Control Block. For the induction motor control, the modeling and simulation is carried out with MATLAB/SIMULINK software. For the modeling 11kW, 400V induction motor is used and parameters of induction motor are shown in table 1.

Rated Power, kW	11
Rated Voltage, V	400
Rated speed, rpm	2460
Numbers of pole (p)	4 poles
Stator resistance (r ₁)	0.35 Ω
Stator reactance (x ₁)	0.88 Ω
Rotor resistance (r ₂)	0.4 Ω
Rotor reactance (x ₂)	1.67 Ω
Magnetizing reactance (x _m)	1.209 Ω

V. Result

The vector control drive for 11 kW three-phase squirrel-cage inductions motor is shown in figure 7. In this drive, the speed is set at 750 rpm and the flux reference is maintained at 0.8. At 0.6 sec the load torque change from no-load to 3.48 Nm, at 1.8 sec the load torque change from 3.49 Nm to 17.4 Nm, at 3 sec the load change from 17.4 Nm to 41.76 Nm, at 4.2 sec the load torque change from 3.48 Nm and at 5.4 sec the load torque change from 3.48 Nm to 0. The resultant three-phase current of vector control of induction motor is shown in figure 10. The load is increased at 0.6 sec, 1.8 sec, 3 sec and decreased at 4.2 sec, 5.4 sec. In this case it seen that, when the load on the motor is increased the motor currents are increased and when the load on the motor is decreased the motor currents are decreased. At maximum load torque (41.76 Nm), the currents are reaching to 18 A.



I in Sci Figure.10 Three-phase Currents Response of Vector

Figure 11 shows the rotor speed of the machine at different load torque. This demonstrates that high dynamic performance speed response to change in demand torque. The sudden application of the load on the motor shaft cause a small dip or rise in the rotor speed, which recovers quickly resulting in zero steady state speed error. In figure 11, the speed reaching to the desired speed at 0.2 sec and is loaded 3.48 Nm, the speed decreases to the 745 rpm and return to the desired speed in 0.1 sec. When the load torque is changed from 3.8 Nm to 17.4 Nm, the speed decreases to the 710 rpm and return to the desired speed in 0.2 sec. When the load torque is changed from 17.4 Nm to 41.76 Nm, the speed decreases till 690 rpm and return to the desired speed in 0.3 sec. When the load torque is changed from 41.76 Nm to 3.48 Nm, the speed increases till 850 rpm and return to the desired speed in 0.3 sec. When the load torque is changed from 3.8 Nm to 0 for no load, the speed increases to the 755 rpm and return to the desired speed in 0.1 sec. It is seem that the speed responses were smooth at different load torques and the speed follow perfectly the speed reference. The speed response is fast, accurate and gives a good result for variable load torque of induction motor.

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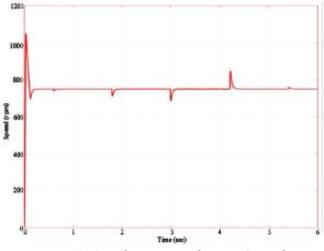


Figure.11 Speed Response of Vector Control

Figure 12 shows the resultant torque response of vector control of three-phase squirrel-cage induction motor.

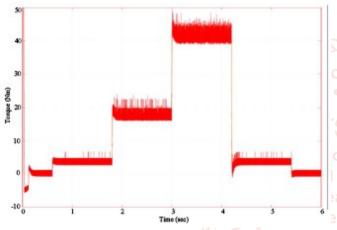


Figure.12 Torque Response of Vector Control

An increase and decrease of the load on the shaft of the motor are developing increase and decrease of electromagnetic torque. When the load torque is suddenly changed, there is the spike torque (it reaches 49 Nm) that carries more current. According to the switching pulse three level bridge switches turned on and off simultaneous, step input is given for as mechanical input. In this method, the deviation of the speed due to the load is so small and speed returns to the desired speed in a very small time.

VI. Conclusion

This paper presents the speed control of induction motor using vector control method was implemented using MATLAB/SIMULINK. In vector control system, a closed loop speed control technique is used for induction motor. The induction motor control system based on vector control method produces the best speed error and no steady state error. Therefore, the results of vector control system are able to perfect the stability of the speed variation and less error speed for induction motor.

References

- [1] Rakesh, P.: *AC Induction Motor Fundamental*, AN 887Microchip Technology Inc., (2003).
- [2] Krishnan, R.: *Electric Motor Drives Modeling, Analysis and Control*, Prentice Hall, Inc., Upper Saddle River, New Jersey 07458, (2001).
- [3] Sprecher, S. A. G. R. A.: Application Basics of Operation of Three-phase Induction Motors, (1996).
- [4] Ashfaq, A.: *Power Electronics for Technology, Hall International*, Inc., International Edition, (1999).
- [5] Ong, C. M.: *Dynamic simulation of electric machinery: using MATLAB/SIMULINK*, vol. 5, Prentice Hall PTR Upper Saddle River, NJ, (1998).
- [6] Chee-Mun, O.: *Dynamic Simulation of Electric Machinery using Matlab/Simulink*, A Simon and Schuster Company, Upper Saddle River, New Jersey, (1997).
- [7] Wang, X., Yang, Y. and Liu, W.: Simulation of vector controlled adjustable speed System of induction motor based on Simulink, pp. 2563-2566,(2011).